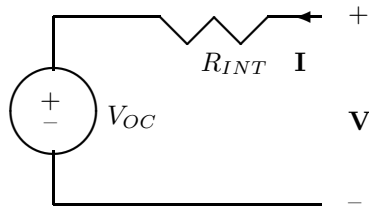
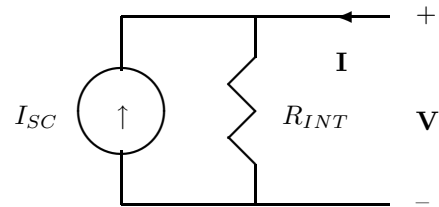


THM: Take *any* network of ideal voltage and current sources and resistors. Take any 2 points in the network and connect wires to them \rightarrow device. Then the i-v characteristic of this device is the same as that of its:

Thevenin equivalent:



Norton equivalent:



1. **Exception:** Pure non-zero current source has no Thevenin equivalent.
Exception: Pure non-zero voltage source has no Norton equivalent.
2. **Why?** $V = V_{OC} + IR_{INT} \Leftrightarrow I = V/R_{INT} - I_{SC}$: Connect up I source, solve *node equations* \rightarrow V depends on I by linear+constant function.
3. **So what?** If you don't care about any *internal* voltages or current, replace circuit with its Thevenin/Norton equivalent simplifies analysis.
4. **Modelling:** We'll use these to *model* batteries & amplifier outputs.
5. **How to compute?** Do **any 2** (easiest 2) of the following 3 things:
 - a. **Open-circuit voltage V_{OC} :** Simply measure voltage with $I = 0$.
 - b. **Short-circuit current I_{SC} :** Clamp a short across the terminals $V = 0$ and measure the current flowing *out of* the "+" terminal.
 - c. **Internal resistance R_{INT} :** First *set all independent sources to zero* (voltage sources \rightarrow shorts; current sources \rightarrow open (gaps)) and measure or compute the resistance between the terminals.

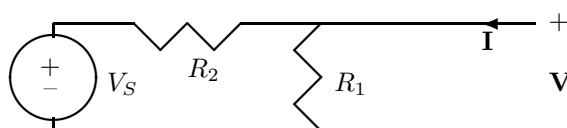
Then: $V_{THEVENIN} = V_{OC}$; $I_{NORTON} = I_{SC}$; $R_{INT} = V_{OC}/I_{SC}$.

EX#1: Compute the Thevenin and Norton equivalents of the **voltage divider:**

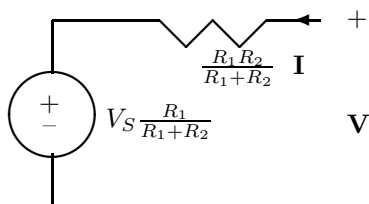
$$V_{OC}: V_{OC} = V_S \frac{R_1}{R_1 + R_2}$$

$$I_{SC}: I_{SC} = V_S / R_2$$

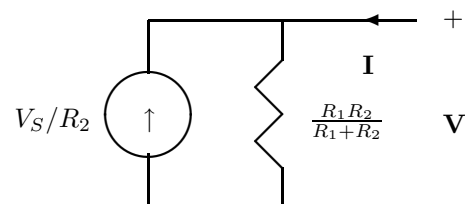
$$R_{INT}: R_{INT} = R_1 \parallel R_2$$



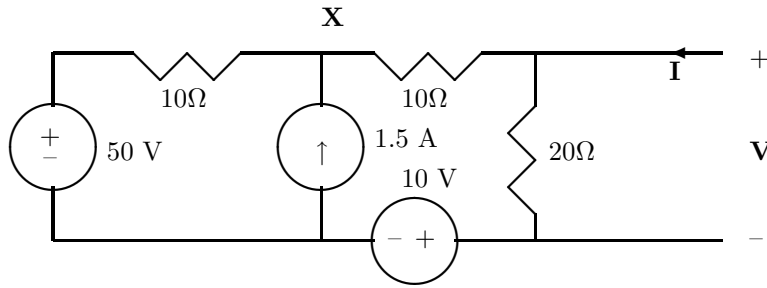
Thevenin equivalent:



Norton equivalent:



EX#2: Compute the Thevenin and Norton equivalents of the circuit shown:



$$V_{OC}: \text{Node equation at } X \rightarrow \frac{X-50}{10} + \frac{X-10}{10+20} = 1.5 \rightarrow X = 51.25V.$$

$$\text{Voltage divider (look carefully)} \rightarrow V_{OC} = \frac{20}{20+10}(51.25 - 10) = 27.5V.$$

$$I_{SC}: \text{Node} \rightarrow \frac{X-50}{10} + \frac{X-10}{10+0} = 1.5 \rightarrow X = 37.5V \rightarrow I_{SC} = \frac{37.5-10}{10} = 2.75A.$$

R_{INT} : Set current source $\rightarrow 0 \Leftrightarrow$ open; voltage sources $\rightarrow 0 \Leftrightarrow$ short:

$$R_{INT} = 20 \parallel (10 + 10) = 10\Omega. \text{ Check: } \frac{V_{OC}}{I_{SC}} = \frac{27.5V}{2.75A} = 10\Omega = R_{INT}.$$

Applications of Thevenin and Norton Equivalents:

1. A battery or stereo output can be modelled by its Thevenin equivalent: The ideal output voltage V_{OC} with an **internal resistance** R_{INT} .

EX: You test a 1.5V battery with a voltmeter and get 1.5V. But when you put it in a flashlight, it doesn't work! Now voltmeter reads 0.5V! Why?

Sol'n: Connect load \rightarrow *voltage division* between R_{INT} and R_L . Bulb: 5Ω .

$$\text{Get } 0.5 = (1.5) \frac{5}{5+R_L} \rightarrow R_L = 10\Omega = \text{internal resistance of battery.}$$

Ideal: $R_{INPUT} \rightarrow \infty$ (draws no current); $R_{OUTPUT} = 0$ (R_{INT} of output).

2. Maximum Power Transfer \Leftrightarrow Load Matching:

Given: Fixed Thevenin equivalent V_{OC} and R_{INT} of stereo amplifier output.

Want: Variable R_L (speaker). What R_L maximizes power dissipated in *load*?

Note: ($R_L=0$) $\rightarrow I_L^2 R_L=0$; ($R_L \rightarrow \infty$) $\rightarrow V_L^2 / R_L=0$. Want intermediate R_L .

Sol'n: Power dissipated in load $= I_L^2 R_L = \left(\frac{V_{OC}}{R_{INT}+R_L} \right)^2 R_L$. Minimize wrt R_L :

$$\frac{d}{dR_L} \left[\left(\frac{V_{OC}}{R_{INT}+R_L} \right)^2 R_L \right] = 0 \rightarrow R_L = R_{INT}: \text{Match load to source.}$$

EX: Stereo has $R_{INT} = 8\Omega \rightarrow$ use 8Ω speakers, not (say) 16Ω speakers.

Mechanical Analogue: shifting gears in car or bicycle.

3. Circuit with *nonlinear* device: Thevenin of circuit "seen" by device.

EX: See Problem Set #5. Try solving that *without* Thevenin equivalent!