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**EXAMPLES OF FIR DIGITAL FILTERS**


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**FIR:** FIR=Finite Impulse Response:  $h[n]$  has finite *duration* and *support*.

**Form:**  $y[n] = b_0x[n] + b_1x[n-1] + b_2x[n-2] + \dots + b_Mx[n-M]$ . Order= $M$ .

**h[n]:**  $h[n] = b_n$  for  $0 \leq n \leq M$ ;  $h[n] = 0$  otherwise. Assume  $h[n]$  is real here.

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**Frequency response:**  $H(e^{j\omega}) = b_0 + b_1e^{-j\omega} + b_2e^{-j2\omega} + \dots + b_Me^{-jM\omega}$ .

$e^{j\omega_0 n} \rightarrow \overline{FIR} \rightarrow H(e^{j\omega_0})e^{j\omega_0 n}$ , implying

$\cos(\omega_0 n) \rightarrow \overline{FIR} \rightarrow |H(e^{j\omega_0})| \cos(\omega_0 n + \arg[H(e^{j\omega_0})])$

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**Properties of  $H(e^{j\omega})$ :**  $H(e^{j\omega})$  **periodic** in  $\omega$  with period  $2\pi$ .

**Conjugate symmetry:**  $H(e^{-j\omega}) = H^*(e^{j\omega})$ .

**Implies: Gain is even function:**  $|H(e^{j\omega})| = |H(e^{-j\omega})|$ .

**Phase is odd function:**  $\arg[H(e^{-j\omega})] = -\arg[H(e^{j\omega})]$ .

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**Notch filter:**  $h[n] = \{1, -2\cos(\omega_0), 1\} \rightarrow H(e^{j\omega}) = [2\cos(\omega) - 2\cos(\omega_0)]e^{-j\omega}$ .

Implement using  $y[n] = x[n] - 2\cos(\omega_0)x[n-1] + x[n-2]$ .

**Does:** Eliminates component at a single frequency  $\omega_0$  from input.

**Why?** Eliminate interference at a single frequency, e.g., 60 Hz “hum.”

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**Comb filter:**  $h[n] = \{1, 1, 1 \dots 1\} \rightarrow H(e^{j\omega}) = \frac{e^{-j\omega(M+1)} - 1}{e^{-j\omega} - 1} = \frac{\sin(\frac{M+1}{2}\omega)}{\sin(\frac{\omega}{2})} e^{-j\omega M/2}$ .

Implement using  $y[n] = x[n] + x[n-1] + \dots + x[n-M]$ .

**Does:** Eliminates components at frequencies  $\pm \frac{2\pi}{M+1}, \pm \frac{4\pi}{M+1} \dots \pm \frac{M\pi}{M+1}$ .

**Why?** Eliminate interference at **harmonics** of a single frequency  $2\pi/(M+1)$ .

e.g., Sawtooth wave interference with period  $(M+1)$  has these harmonics.

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**Ideal LPF:**  $h[n] = \frac{\sin(Bn)}{\pi n} \rightarrow H(e^{j\omega}) = 1$  for  $0 < |\omega| < B$ ;  $= 0$  for  $B < |\omega| < \pi$ .

Implement using  $y[n] = \sum_{i=-\infty}^{\infty} \frac{\sin(Bi)}{\pi i} x[n-i]$ ; truncate the sum.

**Does:** Low-pass filter; eliminates frequencies above  $B$  (periodic; period  $2\pi$ ).

**Why?** Filter out high-frequency noise from a low-frequency signal (smooth).

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**APPLICATION TO ELECTROCARDIOGRAM (HEART) SIGNALS**


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**Given:**  $x(t)$ =EKG signal; periodic (you hope!) at  $60 \frac{\text{BEATS}}{\text{MINUTE}} = 1 \frac{\text{BEAT}}{\text{SECOND}}$ .

**Goal:** Filter out 60 Hz interference from electrical outlet wires in lab.

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**Signal:**  $x(t)$  period=1 second  $\rightarrow$  fundamental=1 Hz  $\rightarrow$  harmonics=2,3... Hz.

**Huh?**  $x(t) = \underbrace{c_0}_{\text{DC}} + \underbrace{c_1 \cos(2\pi t + \theta_1)}_{\text{FUNDAMENTAL}} + \underbrace{c_2 \cos(4\pi t + \theta_2)}_{\text{1ST HARMONIC}} + \underbrace{c_3 \cos(6\pi t + \theta_3)}_{\text{2ND HARMONIC}} \dots$

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**Sample:** at 1 kHz  $\rightarrow \Delta = 0.001$  second  $\rightarrow t = 0.001n \rightarrow x[n] = x(t = 0.001n)$ .

**Spectrum:** of sampled signal  $x[n] = x(0.001n)$  is periodic in  $f$  with period 1 kHz.

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**Notch filter:**  $y[n] = x[n] - 2\cos(2\pi \frac{60}{1000})x[n-1] + x[n-2]$  eliminates 60 Hz “hum.”

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**ARMA DIFFERENCE EQUATIONS**


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**MA:**  $y[n] = b_0x[n] + b_1x[n-1] + \dots + b_qx[n-q]$  (Moving Average)

**Huh?** Present output=weighted average of  $q+1$  *most recent* inputs.

**Note:** Equivalent to  $y[n] = b[n] * x[n]$  where  $b[k] = b_k, 0 \leq k \leq q$ .

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**AR:**  $y[n] + a_1y[n-1] + \dots + a_py[n-p] = x[n]$  (AutoRegression)

**Huh?** Present output=weighted sum of  $p$  *most recent* **outputs**.

**Note:** Compute  $y[n]$  *recursively* from its  $p$  most recent values.

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$$\text{ARMA: } \underbrace{\sum_{i=0}^p a_i y[n-i]}_{\text{AUTOREGRESSIVE}} = \underbrace{\sum_{i=0}^q b_i x[n-i]}_{\text{MOVING AVERAGE}} \begin{cases} \text{MA} \Leftrightarrow \text{FIR (Finite Impulse)} \\ \text{AR} \rightarrow \text{IIR (Infinite Impulse)} \\ \text{ARMA} \rightarrow \text{IIR (Response)} \end{cases}$$


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**Note:** Difference equation  $\sim$  *differential equation* in continuous time:

$$\left( \frac{d^p}{dt^p} + a_1 \frac{d^{p-1}}{dt^{p-1}} + \dots + a_p \right) y(t) = \left( \frac{d^q}{dt^q} + b_1 \frac{d^{q-1}}{dt^{q-1}} + \dots + b_q \right) x(t).$$

**Note:** Coefficients  $a_i$  and  $b_i$  are *not directly* analogous here to  $a_i$  and  $b_i$  above.

**Note:** Linear time-invariant in both cases since all coefficients indpt. of time.

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**EXAMPLES OF IIR FILTERS**


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$$1. h[n] = ba^n u[n] \Leftrightarrow H(z) = b \frac{z}{z-a} \frac{z^{-1}}{z^{-1}} \Leftrightarrow y[n] - ay[n-1] = bx[n] \text{ [1}^{st}\text{-order].}$$


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$$2. h[n] = (c_1 p_1^n + c_2 p_2^n) u[n] \Leftrightarrow H(z) = \frac{c_1 z}{z-p_1} + \frac{c_2 z}{z-p_2} = \frac{(c_1+c_2)z^2 - (c_1 p_2 + c_2 p_1)z}{z^2 - (p_1+p_2)z + (p_1 p_2)}$$

$$\Leftrightarrow y[n] - (p_1+p_2)y[n-1] + (p_1 p_2)y[n-2] = (c_1+c_2)x[n] - (c_1 p_2 + c_2 p_1)x[n-1]$$


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$$2a. h[n] = 2 \cos(\omega_o n) u[n] = (e^{j\omega_o n} + e^{-j\omega_o n}) u[n] \quad [(2, 1)^{nd}\text{-order ARMA}]$$

$$\Leftrightarrow y[n] - 2 \cos(\omega_o) y[n-1] + y[n-2] = 2x[n] - 2 \cos(\omega_o) x[n-1].$$


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$$2b. h[n] = 6\left(\frac{1}{2}\right)^n u[n] + 8\left(\frac{1}{3}\right)^n u[n] \text{ can be implemented by: } [8\left(\frac{1}{2}\right) + 6\left(\frac{1}{3}\right) = 6]$$

$$y[n] - \frac{5}{6}y[n-1] + \frac{1}{6}y[n-2] = 14x[n] - 6x[n-1] \text{ [(2, 1)^{nd}\text{-order ARMA].}$$


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**SO WHY BOTHER TO USE IIR FILTERS?**


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**Goal:** Eliminate 60 Hz “hum” in a continuous-time signal sampled at 250 Hz.

**FIR:** Notch:  $y[n] = x[n] - 2 \cos(2\pi \frac{60}{250})x[n-1] + x[n-2]$ . See below left.

**IIR:** ARMA:  $y[n] - 1.98 \cos(2\pi \frac{60}{250})y[n-1] + 0.98y[n-2] \text{ [(2, 2)^{nd}\text{-order}]}$   
 $= x[n] - 2 \cos(2\pi \frac{60}{250})x[n-1] + x[n-2]$ . See below right.

**Point:** The IIR filter has a *much* sharper frequency response than the FIR filter.

